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DESCRIPTION

IPM ELECTRIC ROTATING MACHINE

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Technical Field

The present invention is related to IPM (Interior Permanent Magnet) electric rotating machines, such as IPM motors and IPM generators.

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Background Art

The IPM motor is a brushless motor having permanent magnets embedded in a rotor core. The IPM motor is advantageous in large output torque per volume, and reduced input voltage. These advantages make it preferable to apply the IPM motor to drive motors of electric vehicles.

An IPM motor also functions as a generator, when externally fed with motive energy. The fact that an IPM motor also functions as a generator is especially important for application to electric vehicles. Hereinafter, IPM motors and IPM generators are collectively referred to as IPM electric rotating machines, when it is unnecessary to distinguish IPM motors and IPM generators.

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The IPM electric rotating machine is desired to generate a large output torque. An IPM motor structure for generating a large output torque is disclosed in Japanese Laid Open Patent Application

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No. Jp 2002-153033A. In the disclosed IPM motor, permanent magnets of the field magnet system are shallowly embedded in a rotor core. Such structure enables generating an increased magnet torque and an auxiliary reluctance torque, and thereby effectively increases the output torque of the IPM motor. The above-mentioned document discloses that the increase in the flux density of the flux applied to armature coils is preferable for increasing the magnet torque. Additionally, the above-mentioned document discloses that it is preferable that the permanent magnets are shallowly embedded in the rotor core, and thereby the q-axis inductance and the d-axis inductance satisfy the following relation:

$$0 \leq (L_q - L_d) / L_d < 0.3.$$

Disclosure of Invention

An object of the present invention is to provide a rotor structure of an IPM electric rotating machine for achieving further increased output torque.

In an aspect of the present invention, an IPM electric rotating machine is composed of a stator, and a rotor including a rotor core and a plurality of permanent magnets functioning as a field magnet system. The rotor has a side face opposed to the stator, and the permanent magnets each have a pole face opposed to the side face. The permanent magnets are embedded so that a maximum value of a distance

from the pole face to the side face satisfies the following formulas (1a) and (1b) which are represented by a radius r of the rotor, and a number of poles of the field magnet system:

5 $x \leq D/10$, and $\dots(1a)$

$D = 2\pi r/n_1$, and $\dots(1b)$

Additionally, adjacent two of the permanent magnets, which function as adjacent two poles of the field magnet system are spaced apart so that the following
10 formula (2) is satisfied, which is described using a q-axis inductance L_q , and d-axis inductance L_d :

$$0.3 < (L_q - L_d)/L_d. \quad \dots(2)$$

In the IPM electric rotating machine thus designed, the magnet torque is large due to the fact that the
15 permanent magnets are shallowly embedded.

Additionally, the volume of inter-magnet core portions of the rotor core positioned between adjacent two of the permanent magnets is large in IPM electric rotating machine, which increases the
20 reluctance torque exerted on the inter-magnet core portions. These effects allow the IPM electric rotating machine to increase the output torque, which is the sum of the magnet torque and the reluctance torque.

25 When the stator is fed with a three-phase current, it is preferable that the number of poles n_1 of the field magnet system and a number of slots n_2 provided for the stator are any one of the following

combinations:

$$n_1 = 12, n_2 = 9,$$

$$n_1 = 14, n_2 = 12,$$

$$n_1 = 16, n_2 = 12,$$

5 $n_1 = 16, n_2 = 18,$

$$n_1 = 20, n_2 = 15,$$

$$n_1 = 20, n_2 = 18,$$

$$n_1 = 20, n_2 = 21,$$

$$n_1 = 22, n_2 = 24,$$

10 $n_1 = 24, n_2 = 18,$

$$n_1 = 24, n_2 = 27,$$

$$n_1 = 26, n_2 = 24,$$

$$n_1 = 28, n_2 = 24, \text{ and}$$

$$n_1 = 30, n_2 = 27.$$

15 These combinations remarkably improve the characteristics of the IPM electric rotating machine in which the permanent magnets are shallowly embedded.

20 When the stator is fed with a five-phase current, the number of poles n_1 of the field magnet system and a number of slots n_2 provided for the stator are any one of the following combinations:

$$n_1 = 12, n_2 = 10,$$

$$n_1 = 14, n_2 = 10,$$

25 $n_1 = 22, n_2 = 20,$

$$n_1 = 18, n_2 = 20,$$

$$n_1 = 24, n_2 = 20,$$

$$n_1 = 26, n_2 = 20,$$

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$$n_1 = 28, n_2 = 20,$$

$$n_1 = 26, n_2 = 30, \text{ and}$$

$$n_1 = 28, n_2 = 30.$$

These combinations remarkably improve the
5 characteristics of the IPM electric rotating machine
in which the permanent magnets are shallowly
embedded.

The present invention provides a rotor
structure of an IPM electric rotating machine for
10 achieving further increased output torque.

Brief Description of Drawings

Fig. 1 illustrates a first embodiment of an IPM
electric rotating machine in accordance with the
15 present invention;

Fig. 2 is an enlarged view of a rotor 12;

Fig. 3 is a view illustrating an arrangement of
permanent magnets 18; and

Fig. 4 illustrates a second embodiment of an IPM
20 electric rotating machine in accordance with the
present invention.

Best Mode for Carrying Out the Invention

Embodiments of the IPM electric rotating machine
25 in accordance with the present invention will be
described below with reference to the attached
drawings.

(First Embodiment)

In a first embodiment of the present invention, as shown in Fig. 1, an IPM motor 10 is composed of a stator 11 and a rotor 12. The stator 11 is opposed to the rotor side face 12a of the rotor 12. The stator 11 applies a torque to the rotor 12 through the electromagnetic effect, and thereby rotates the rotor 12 around the center axis 12b. The IPM motor 10 also functions as a generator, when externally fed with motive power.

The torque applied to the rotor 12, that is, the output torque from the IPM motor 10 includes components of both of the magnet torque and the reluctance torque. The IPM motor 10 is designed to enhance the sum of the magnet torque and the reluctance torque (that is, the output torque) through optimization of the structure of the rotor 12. Descriptions are given of the structures of the stator 11 and the rotor 12 in the following.

The stator 11 is composed of armature teeth 13₁ to 13₁₂. In the following, the armature teeth 13₁ to 13₁₂ may be referred to as armature teeth 13, when it is unnecessary to distinguish the armature teeth 13₁ to 13₁₂ one another. The armature teeth 13 are circumferenced and spaced at constant intervals. A slot 14 is formed between every adjacent two armature teeth 13. This implies that the slots 14 are circumferenced and spaced at constant intervals.

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Armature coils 15_1 to 15_{12} are wound around the armature teeth 13_1 to 13_{12} , respectively. A three-phase armature current is fed to the armature coils 15_1 to 15_{12} to generate a rotating magnetic field within the stator 11. In detail, A U-phase current is fed to the armature coils 15_1 , 15_2 , 15_7 , and 15_8 , a V-phase current is fed to the armature coils 15_3 , 15_4 , 15_9 , and 15_{10} , and a W-phase current is fed to the armature coils 15_5 , 15_6 , 15_{11} , and 15_{12} . The armature coils 15_1 , 15_4 , 15_5 , 15_8 , 15_9 , and 15_{12} are wound in a first direction (for example, clockwise), while the armature coils 15_2 , 15_3 , 15_6 , 15_7 , 15_{10} , and 15_{11} are wound in a second direction opposite to the first direction (for example, counterclockwise). The armature coils 15_1 to 15_{12} may be referred to as armature coils 15, when it is unnecessary to distinguish the armature coils 15_1 to 15_{12} , one another.

The armature coils 15 are wound around the armature teeth 13 with concentrated winding. Winding the armature coils 15 with concentrated winding preferably increases the torque of the IPM motor 10 per volume.

The rotor 12 is composed of a shaft 16 and a rotor core 17. The shaft 16 is rotatably supported by roller bearings (not shown). The rotor core 17 is rigidly fixed to the shaft 16, rotating with the shaft 16. The rotor core 17 is formed of magnetic material,

such as silicon steel.

Permanent magnets 18 are inserted into the rotor core 17. Each of the permanent magnets 18 functions as a pole of the field magnet system of the rotor 12, generating magnetic flux in the radial direction of the rotor 12. Adjacent two permanent magnets 18 generates magnetic flux in the opposite directions; that is, the polarities of adjacent two permanent magnets 18 are opposite. In this embodiment, the number of the permanent magnets 18, that is, the number of pole n_1 is 14.

As shown in Fig. 2, the rotor core 17 includes portions 17a positioned outside the permanent magnets 18 in the radial direction (flux inducing portions 17a). The flux inducing portions 17a are connected with the main core body 17b on the ends positioned in the circumferential direction. The existence of the flux inducing portions 17a is important for achieving weak field control. As is well known in the art, the weak field control, which advances the phase of the armature current, is implemented when an IPM motor is operated at a high revolution speed. The flux inducing portions 17a facilitates the implementation of the weak field control. It is hard to implement the weak field control for an SPM (Surface Permanent Magnet) motor, which does not include flux inducing portions 17a.

Differently from typical IPM motors, the IPM

motor in this embodiment is shallow in the embedding depth of the permanent magnets 18 from the rotor side face 12a, (that is, the maximum value of the distance from the pole faces 18a positioned outward in the radial direction to the rotor side face 12a). Quantitatively, the permanent magnets 18 are embedded at positions at which the embedding depth x satisfies the following formulas (1a) and (1b) which are represented by the radius r of the rotor 12, and the number of the poles n_1 :

$$x \leq D/10, \text{ and } \dots (1a)$$

$$D = 2\pi r / n_1. \dots (1b)$$

The shallowly embedded permanent magnets 18 are effective for making use of the magnet torque of the IPM motor 10, as well as achieving the weak field control. The shallowly embedded permanent magnets 18 allow much of the flux generated by the permanent magnets 18 to be applied to the armature coils 15, and thereby enhances the magnet torque. The use of the magnet torque is effective for increasing the output torque.

Additionally, as shown in Fig. 3, the IPM motor in this embodiment achieves an increase in the output torque through making effective use of the reluctance torque exerted on inter-magnet core portions 17c of the rotor core 17, which are positioned between adjacent permanent magnets 18.

Specifically, in order to increase the

reluctance torque exerted on inter-magnet core portions 17c, the width of the pole faces 18a of the permanent magnets 18 is reduced in the circumferential direction to intentionally increase the distance between the adjacent permanent magnets 18. Such arrangement of the permanent magnets 18 increases the volume of the inter-magnet core portions 17c, and thereby increases the reluctance torque exerted on inter-magnet core portions 17c.

Qualitatively, adjacent two of the permanent magnets 18 are spaced apart so that the following formula (2) holds:

$$0.3 < (L_q - L_d) / L_d, \quad \dots (2)$$

where L_q is the q-axis inductance of the rotor 12, and the L_d is the d-axis inductance thereof.

The technique presented in this embodiment, which makes use of the reluctance torque exerted on the inter-magnet core portions 17c, is based on a technical idea completely different from the technique disclosed in the document mentioned in the description of the Background Art. The above-described document discloses that it is preferable for the increase in the magnet torque to enhance the flux density of the flux applied to the armature coils. The IPM motor in this embodiment, on the contrary, the width of the pole faces 18a of the permanent magnets 18 is intentionally reduced in the circumferential direction, and thereby the flux

applied to the armature coil 15 is reduced. This results in that the reduction of the magnet torque; however, the IPM motor in this embodiment achieves the increase in the reluctance torque exerted on the inter-magnet core portions 17c due to the increase in the distance between adjacent two of the permanent magnets 18, and thereby increases the output torque as a whole.

The shallowly embedded permanent magnets 18 are effective for the structure in which the distance between two permanent magnets 18 is increased to make effective use of the reluctance torque. The reluctance torque of the IPM motor 10 in this embodiment is represented by the following formula (3):

$$T_R = K(L_q - L_d)I_q \cdot I_d, \quad \dots (3)$$

where K is a constant, and I_q and I_d are the q-axis and d-axis current through the armature coils 15, respectively. The increase in the distance between adjacent permanent magnets 18 causes an increase in the q-axis inductance L_q , and therefore enhances the output torque as is understood from the formula (3). Additionally, the shallowly embedded permanent magnets 18 cause a decrease in the d-axis inductance L_d . As is understood from the formula (3), the decrease in the d-axis inductance L_d increases the reluctance torque T_R . Furthermore, the decrease in the d-axis inductance L_d causes an increase in the

d-axis current I_d , and therefore enhances the reluctance torque T_R as is understood from the formula (3).

As explained above, in this embodiment, the permanent magnets 18 are shallowly embedded, and the distance between adjacent permanent magnets 18 are increased. This achieves the increase in the reluctance torque exerted on the inter-magnet core portions 17, and thereby increases the output torque of the IPM motor 10. Additionally, the shallowly embedded permanent magnets 18 cause the decrease in the d-axis inductance L_d , and thereby further increases the reluctance torque exerted on the inter-magnet portions 17.

As thus described, the IPM motor 10 in this embodiment makes effective use of both of the magnet torque and the reluctance torque exerted on the inter-magnet core portions 17c, differently from typical IPM motors. This results from the shallowly embedded permanent magnets 18 and the intentionally increased distance between adjacent permanent magnets 18.

In order to make effective use for the specialty of the IPM motor 10 thus designed, it is preferable that the number of poles of the rotor 12 (denoted by n_1), and the number of slots 14, denoted by n_2 (that is, the number of the armature teeth 13) are any one of the following combinations:

$$n_1 = 12, n_2 = 9,$$

$$n_1 = 14, n_2 = 12,$$

$$n_1 = 16, n_2 = 12,$$

$$n_1 = 16, n_2 = 18,$$

$$5 \quad n_1 = 20, n_2 = 15,$$

$$n_1 = 20, n_2 = 18,$$

$$n_1 = 20, n_2 = 21,$$

$$n_1 = 22, n_2 = 24,$$

$$n_1 = 24, n_2 = 18,$$

$$10 \quad n_1 = 24, n_2 = 27,$$

$$n_1 = 26, n_2 = 24,$$

$$n_1 = 28, n_2 = 24, \text{ and}$$

$$n_1 = 30, n_2 = 27.$$

As is well known in the art, the three-phase IPM motor requires that the number of poles n_1 is an even number, and the number of slots n_2 is a multiple of 3, while the number of poles n_1 and the number of slots n_2 are different. Various combinations satisfying these requirements may be allowed for the number of poles n_1 and the number of slots n_2 ; however, the above-described combinations are especially advantageous for the IPM motor 10, which is composed of the shallowly embedded permanent magnets 18. The reason is as follows:

25 Firstly, all these combinations require that the number of poles n_1 is relatively large. As described in the above-mentioned document, the increase in the number of poles n_1 increases the armature-coil-

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applied component of the flux generated by the field magnet system, and thereby increases the magnet torque, which is the main component of the output torque of the IPM motor 10.

5 Secondly, these combinations allow each permanent magnet 18, which functions as each pole of the field magnet system, to be opposed in the front of one of the armature teeth 13. Specifically, the above-described combinations reduce the difference
10 between the number of poles n_1 and the number of slots n_2 down to five or less. This effectively increases the magnet torque, which is the main component of the output torque of the IPM motor 10. The reduced
15 difference between the number of poles n_1 and the number of slots n_2 is also effective for increasing the winding factor. The increased winding factor allows more of the flux generated by the permanent magnets 18 to be applied to the armature coils 15, and thereby increases the magnet torque.
20 Quantitatively, all of the above-described combinations achieve an increase in the winding factor up to 0.94 or more.

 Thirdly, these combinations increase the winding factor for the fundamental harmonic component
25 of the stator magneto motive force, and allow design for the reduction of the winding factor for the higher harmonic component. Therefore, these combinations especially increase the output of the IPM motor 10.

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The above-described combinations, which enjoy all of these advantages, are advantageous for the IPM motor 10, in which the embedding depth of the permanent magnets 18 is shallow.

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(Second Embodiment)

In a second embodiment, the present invention is applied to a five-phase IPM motor 30, as shown in Fig. 4. The use of the five-phase IPM motor is
10 preferable compared to the three-phase IPM motor, because the five-phase IPM motor 30 allows reducing the capacity of the inverter and the capacitance of the capacitor necessary for the drive thereof. The IPM motor 30 is composed of a stator 31, and a rotor
15 32.

The stator 31 is composed of armature teeth 33. The armature teeth 33 are circumferenced and spaced at constant intervals. A slot 34 is formed between every two adjacent armature teeth 33. This implies
20 that the slots 34 are circumferenced and spaced at constant intervals. In this embodiment, the number of the slots 34, denoted by n_2 , is 20. Armature coils 35 are wound around the respective armature teeth 33. The armature coils 35 are fed with a five-phase
25 armature current to generate a rotating magnetic field inside the stator 11.

The structure of the rotor 32 is identical to the rotor 12 in the first embodiment, except for the

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number of the permanent magnets 18. In this embodiment, the number of the permanent magnets 18 (that is, the number of poles of the field magnet system) is 22. The permanent magnets 18 are embedded
 5 at shallow positions at which the embedding depth x satisfies the following formulas (1a) and (1b):

$$x \leq D/10, \quad \dots (1a)$$

$$D = 2\pi r / n_1, \quad \dots (1b)$$

where r is the radius of the rotor 12, and n_1 is the
 10 number of the poles n_1 . Additionally, adjacent two of the permanent magnets 18 are spaced apart so that the following formula (2) holds:

$$0.3 < (L_q - L_d) / L_d, \quad \dots (2)$$

It is preferable that the number of poles of the
 15 rotor 32 (denoted by n_1), and the number of slots 34, denoted by n_2 (that is, the number of the armature teeth 33) are any one of the following combinations:

$$n_1 = 12, \quad n_2 = 10,$$

$$n_1 = 14, \quad n_2 = 10,$$

$$20 \quad n_1 = 22, \quad n_2 = 20,$$

$$n_1 = 18, \quad n_2 = 20,$$

$$n_1 = 24, \quad n_2 = 20,$$

$$n_1 = 26, \quad n_2 = 20,$$

$$n_1 = 28, \quad n_2 = 20,$$

$$25 \quad n_1 = 26, \quad n_2 = 30, \text{ and}$$

$$n_1 = 28, \quad n_2 = 30.$$

As is well known in the art, the five-phase IPM motor requires that the number of poles n_1 is an even number,

and the number of slots n_2 is a multiple of 10, while the number of poles n_1 and the number of slots n_2 are different. Various combinations satisfying these requirements may be allowed for the number of poles
5 n_1 and the number of slots n_2 ; however, the above-described combinations are, especially advantageous for the IPM motor 30, which is composed of the shallowly embedded permanent magnets 18.

Firstly, all these combinations require that the
10 number of poles n_1 is relatively large. As described in the above-mentioned document, the increase in the number of poles n_1 increases the armature-coil-applied component of the flux generated by the field magnet system, and thereby increases the magnet
15 torque, which is the main component of the output torque of the IPM motor 30.

Secondly, these combinations allow each permanent magnet 18, which functions as each pole of the field magnet system, to be opposed in the front
20 of one of the armature teeth 33. This effectively increases the magnet torque, which is the main component of the output torque of the IPM motor 30. These combinations allow applying more of the flux generated by the permanent magnets 18 to the armature
25 coils 35, and thereby increases the magnet torque.

Thirdly, these combinations increase the winding factor for the fundamental harmonic component of the stator magneto motive force, while allowing

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design for the reduction of the winding factor for the higher harmonic component. Therefore, these combinations especially increase the output of the IPM motor 30.

5 The above-described combinations, which enjoy all of these advantages, are advantageous for the IPM motor 30, in which the embedding depth of the permanent magnets 18 is shallow.

10 It should be noted that each permanent magnet 18, which functions as one pole of the field magnet system, may be composed of a plurality of permanent magnet pieces that generate magnetic flux in the same direction. In this case, bridge portions that couple the flux inducing portions 17a with the main core body 15 17b are provided between the permanent magnet pieces. The bridge portions improves the coupling strength between the flux inducing portions 17a and the main core body 17b, and thereby effectively improves the mechanical strength of the rotor 12.